# Communication Systems II

[KECE322\_01] <2012-2nd Semester>

## Lecture #18 2012.11.7 School of Electrical Engineering Korea University Prof.Young-Chai Ko

# Outline

- Signal design for bandlimited channels
  - The Nyquist criterion

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### PAM Transmission through Bandlimited Baseband Channels

PAM transmit signals

$$v(t) = \sum_{n=-\infty}^{\infty} a_n g_T(t - nT),$$

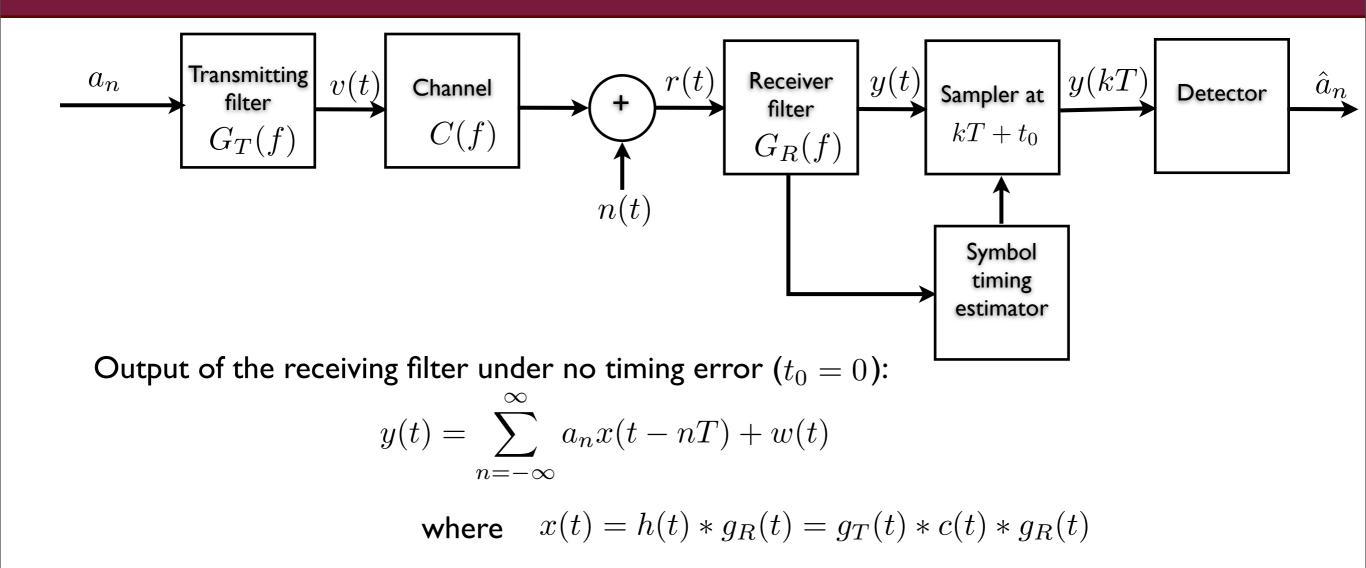
where  $T = \frac{k}{R_b}$  is the symbol interval,  $R_b$  is the bit rate and  $\{a_n\}$  is a sequence

of the amplitude levels corresponding to the sequence of k-bit blocks of information

bits.

Received signals

$$r(t) = \sum_{n=-\infty}^{\infty} a_n h(t - nT) + n(t)$$



Sampled signal

$$y(mT) = \sum_{n=-\infty}^{\infty} a_n x(mT - nT) + w(mT)$$

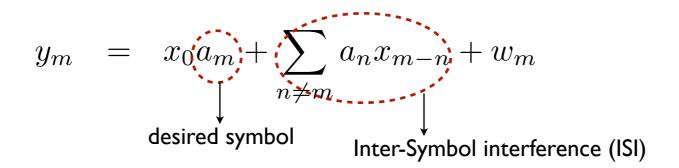
or equivalently,

$$y_m = \sum_{n=-\infty}^{\infty} a_n x_{m-n} + w_m = x_0 a_m + \sum_{n \neq m} a_n x_{m-n} + w_m$$

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#### Note that

$$x(t) = h(t) * g_R(t)$$

if the receiving filter  $g_R(t)$  is matched to h(t), then

$$\begin{aligned} x(0) &\triangleq x_0 &= \int_{-\infty}^{\infty} h(\lambda)h(\lambda) \, d\lambda \\ &= \int_{-\infty}^{\infty} h^2(t) \, dt \\ &= \int_{-\infty}^{\infty} |H(f)|^2 \, df = \int_{-W}^{W} |G_T(f)|^2 |C(f)|^2 \, df = \mathcal{E}_h \end{aligned}$$

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## Signal Design for Bandlimited Channels

ISI signal

$$y_m = x_0 a_m + \sum_{n \neq m} a_n x_{m-n} + w_m$$

Bandlimited channel model

$$C(f) = \begin{cases} C_0 e^{-j2\pi f t_0}, & |f| \le W \\ 0, & |f| > W \end{cases}$$

• Output of the receiving filter

$$X(f) = G_T(f)C(f)G_R(f) = G_T(f)C(f)C_0e^{-j2\pi ft_0}$$

• Assuming 
$$C_0 = 1$$
 and  $t_0 = 0$ 

$$X(f) = G_T(f)C(f), \qquad |f| \le W$$



$$x(nT) = \begin{cases} 1, & n = 0\\ 0, & n \neq 0 \end{cases}$$

which is called Nyquist condition for zero ISI.

Nyquist condition for zero ISI

• A necessary and sufficient condition for x(t) to satisfy

$$x(nT) = \begin{cases} 1, & n = 0\\ 0, & n \neq 0 \end{cases}$$

is that its Fourier transform  ${\boldsymbol X}(f)$  must satisfy

$$\sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right) = T$$

Proof

$$x(t) = \int_{-\infty}^{\infty} X(f) e^{j2\pi ft} df.$$

At the sampling instants t = nT, it becomes

$$\begin{aligned} x(nT) &= \int_{-\infty}^{\infty} X(f) e^{j2\pi f nT} df \\ &= \sum_{m=-\infty}^{\infty} \int_{-(2m-1)/2T}^{(2m+1)/2T} X(f) e^{j2\pi f nT} df \\ &= \sum_{m=-\infty}^{\infty} \int_{-1/2T}^{1/2T} X\left(f + \frac{m}{T}\right) e^{j2\pi f nT} df \\ &= \int_{-1/2T}^{1/2T} \left[\sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right)\right] e^{j2\pi f nT} df \\ &= \int_{-1/2T}^{1/2T} Z(f) e^{j2\pi f nT} df, \end{aligned}$$

where 
$$Z(f) = \sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right)$$

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$$Z(f) = \sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right) \qquad \qquad x(nT) = \int_{-1/2T}^{1/2T} Z(f) e^{j2\pi f nT} df,$$

⋆ Z(f) is periodic function with period  $\frac{1}{T}$ ; therefore it can be expanded in terms of its Fourier series coefficients {z<sub>n</sub>} as

$$Z(f) = \sum_{n = -\infty}^{\infty} z_n e^{j2\pi n fT}$$

where

$$z_n = T \int_{-\frac{1}{2T}}^{\frac{1}{2T}} Z(f) e^{-j2\pi n fT} df.$$

Compare the following two:

$$z_n = T \int_{-\frac{1}{2T}}^{\frac{1}{2T}} Z(f) e^{-j2\pi n fT} df, \text{ and } x(nT) = \int_{-1/2T}^{1/2T} Z(f) e^{j2\pi f nT} df,$$

Then we have:  $z_n = Tx(-nT)$ 

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$$z_n = \begin{cases} T, & n = 0\\ 0, & n \neq 0 \end{cases}$$

since 
$$z_n = Tx(-nT)$$
 and zero ISI condition is  $x(nT) = \begin{cases} 1, & n = 0 \\ 0, & n \neq 0 \end{cases}$ .

• which yields Z(f) = T, symbol duration

or equivalently

$$\sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right) = T.$$

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$$B(f) = \sum_{m = -\infty}^{\infty} X\left(f + \frac{m}{T}\right)$$

• Then the Nyquist criterion is

$$B(f) = T.$$

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Suppose that the channel has a bandwidth of W.

- Then C(f) = 0 for |f| > W; consequently, X(f) = 0 for |f| > W.
- Note that the Nyquist criterion for zero ISI is  $\sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right) = T.$
- We distinguish three cases.

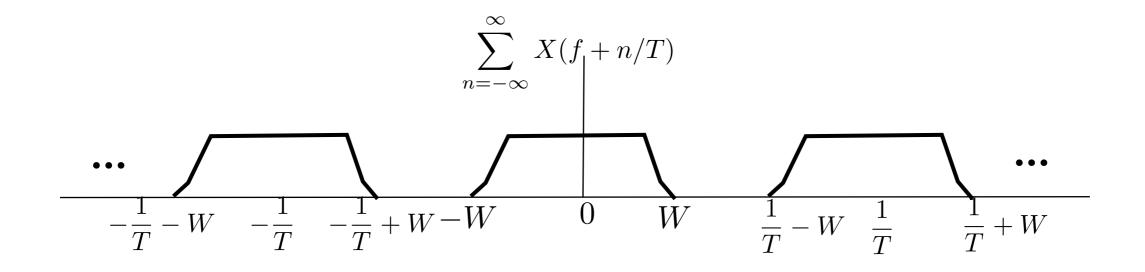
I. When 
$$T < \frac{1}{2W}$$
, or equivalently,  $\frac{1}{T} > 2W$ 

- 2. When  $T = \frac{1}{2W}$
- 3. When  $T > \frac{1}{2W}$

When  $T < \frac{1}{2W}$ , or equivalently,  $\frac{1}{T} > 2W$ ,  $B(f) = \sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right)$  consists of

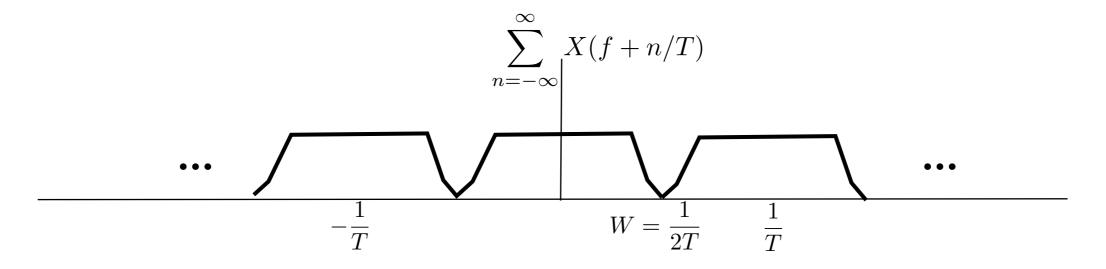
non-overlapping replicas of X(f), separated by 1/T.

• There is no choice for X(f) to ensure  $B(f) \equiv T$  in this case and there is no way that we can design a system with no ISI.



When T = 1/2W, or equivalently, 1/T = 2W, the replication of X(f) separated by 1/T

has the form as below



In this case there exists only one X(f) that results B(f) = T, namely,

$$X(f) = \begin{cases} T, & (|f| < W) \\ 0, & (\text{otherwise}) \end{cases}$$

#### which corresponds to

$$x(t) = \frac{\sin(\pi t/T)}{\pi t/T} \equiv \operatorname{sinc}\left(\frac{\pi t}{T}\right)$$

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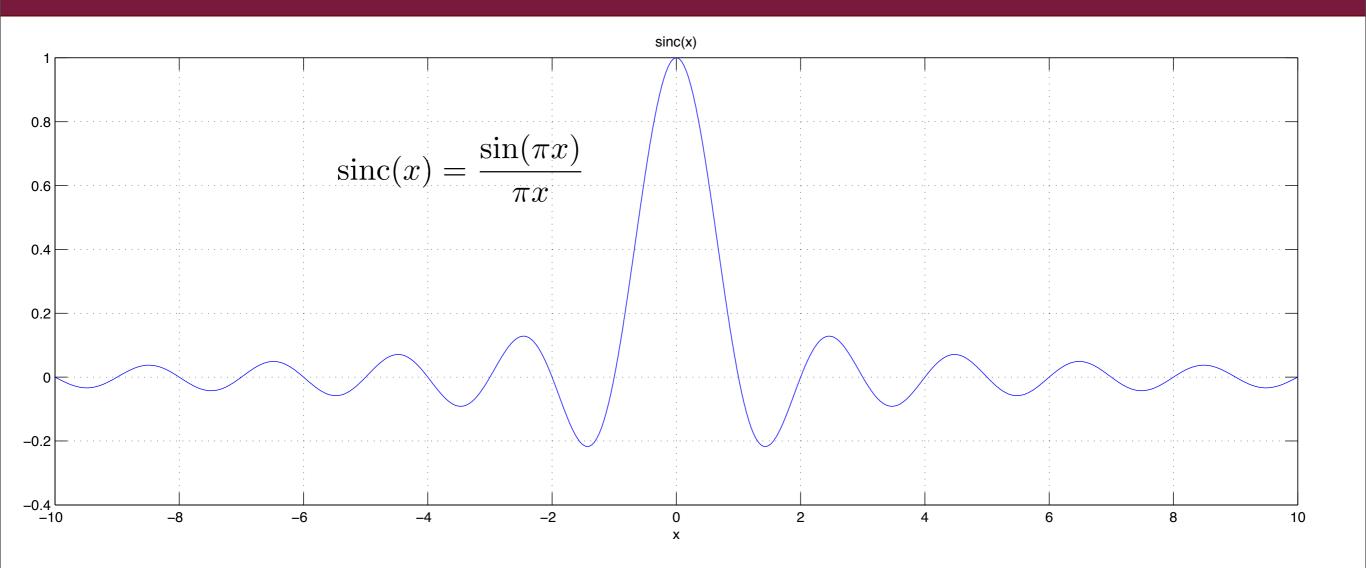
This means that the smallest value of  $\,T\,$  for which transmission with zero ISI is

possible is T = 1/2W, and for this value, x(t) has to be a sinc function.

- The **difficulty** with this choice of x(t) is that it is non-causal and therefore non-realizable.
- To make it realizable, usually a delayed version of it, i.e.,  $\operatorname{sinc}[\pi(t t_0)/T]$  is used and  $t_0$  is chosen such that for t < 0, we have  $\operatorname{sinc}[\pi(t - t_0)/T] \approx 0$ .
- Of course, with this choice of x(t), the sampling time must be shifted to  $mT + t_0$ .

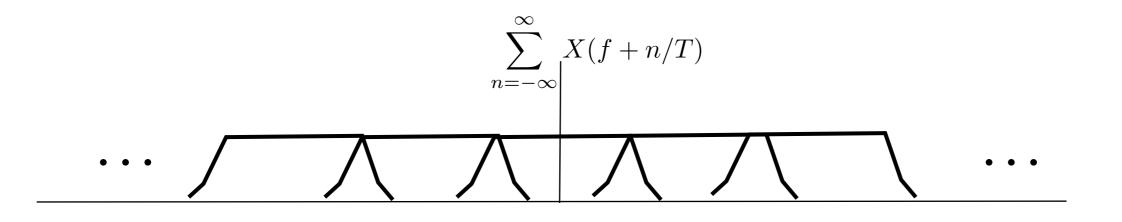
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A second **difficulty** with this pulse shape is that its rate of convergence to zero is low. The tails of x(t) decays as 1/t, consequently, a small mistiming error in sampling the output of the matched filter at the demodulator results in an infinite series of ISI components. When T > 1/2W, B(f) consists of overlapping replications of X(f) separated by 1/T.

In this case, there exists numerous choice for X(f) such that  $B(f) \equiv T$ .



A particular pulse spectrum for the T > 1/2W case, that has desirable spectral

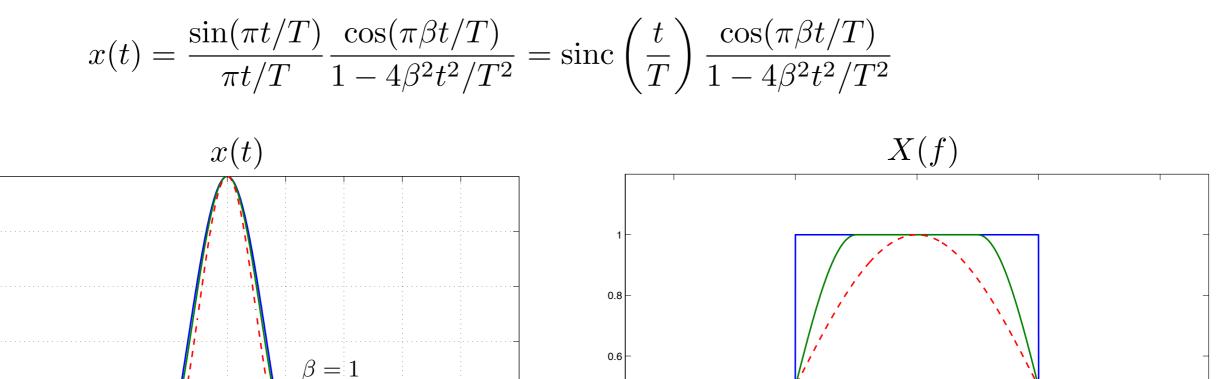
properties and has been widely used in practice is the *raised cosine spectrum*.

$$X_{rc}(f) = \begin{cases} T \\ \frac{T}{2} \left\{ 1 + \cos\left[\frac{\pi t}{\beta} \left( |f| - \frac{1-\beta}{2T} \right) \right] \right\} & \begin{pmatrix} 0 \le |f| \le \frac{1-\beta}{2T} \\ \frac{1-\beta}{2T} \le |f| \le \frac{1+\beta}{2T} \\ |f| > \frac{1+\beta}{2T} \end{pmatrix} \end{cases}$$

where  $0 \le \beta \le 1$  is called roll-off factor.

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0.4

0.2

-Т

 $\beta = 0$ 

0

-0.5T



ЗT

4T

Note that x(t) is normalized so that x(0) = 1.

2T

Т

0

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0.8

0.6

0.4

0.2

-0.2

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 $\beta = 1$ 

т

0.5T

Raised cosine pulse

$$x(t) = \frac{\sin(\pi t/T)}{\pi t/T} \frac{\cos(\pi \beta t/T)}{1 - 4\beta^2 t^2/T^2} = \operatorname{sinc}\left(\frac{t}{T}\right) \frac{\cos(\pi \beta t/T)}{1 - 4\beta^2 t^2/T^2}$$

• For  $\beta = 0$ , the pulse reduces to  $x(t) = \operatorname{sinc}\left(\frac{t}{T}\right)$  and the symbol rate is  $\frac{1}{T} = 2W$ .

• For 
$$\ eta=1,$$
 the symbol rate is  $\ rac{1}{T}=W.$ 

In general, the tails of x(t) decays as  $1/t^3$  for  $\beta > 0$ . Consequently, a mistiming error in sampling leads to a series of ISI components that converges to a finite value.

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