

# KECE321 Communication Systems I

*(Haykin Sec. 3.6)*

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# Summary

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- **Amplitude modulation**
  - Hilbert transform
  - Single-Sideband (SSB) Modulation
    - Generation of SSB modulation
    - Coherent detection
    - Non-coherent detection

# Hilbert Transform

- Consider a filter that simply phase shifts all frequency components of its input by  $-\pi/2$  radians, that is, its transfer function is

$$H(f) = -j\text{sgn}f$$

- Note that

$$|H(f)| = 1, \text{ and } \angle H(f) = \begin{cases} -\pi/2 & f > 0, \\ \pi/2 & f < 0 \end{cases}$$

- Input-Hilbert filter-Output signals



- Let us denote

$$\hat{x}(t) = \mathcal{F}^{-1}[Y(f)]$$

- Then

$$\hat{x}(t) = \mathcal{F}^{-1}[-j\text{sgn}(f)X(f)] = h(t) * x(t)$$

- Now let us calculate the inverse transform of  $h(t)$ .

- Recall  $\mathcal{F}[\text{sgn}(t)] = \frac{1}{j\pi f}$ , then using the duality property we have

$$\mathcal{F}^{-1}[\text{sgn}(f)] = \frac{1}{j\pi(-t)} = \frac{j}{\pi t}$$

- We get the Fourier transform pair

$$\frac{j}{\pi t} \iff \text{sgn}(f) \quad \text{or} \quad \frac{1}{\pi t} \iff -j \text{sgn}(f)$$

- Now we obtain the output of the filter

$$\hat{x}(t) = x(t) * h(t) = \int_{-\infty}^{\infty} \frac{x(\lambda)}{\pi(t - \lambda)} d\lambda$$

- The function  $\hat{x}(t)$  is defined as the Hilbert transform of  $x(t)$  .

- Remarks

- The Hilbert transform corresponds to a phase shift of  $-\pi/2$  .

- The Hilbert transform of  $\hat{x}(t)$

$$\hat{\hat{x}}(t) = -x(t)$$

# Properties of Hilbert Transform

1. Energies are equal

$$|\hat{X}(f)|^2 = |-j\text{sgn}(f)|^2 |X(f)|^2 = |X(f)|^2$$

2. A signal and its Hilbert transform are orthogonal;

$$\int_{-\infty}^{\infty} x(t)\hat{x}(t) dt = 0 \qquad \int_{-\infty}^{\infty} X(f)\hat{X}(f) df = 0$$

# Analytic Signals

- Definition of the analytic signal  $x_p(t)$

$$x_p(t) = x(t) + j\hat{x}(t)$$

- Fourier transform of the analytic signal

$$X_p(f) = X(f) + j[-j\text{sgn}(f)X(f)] = X(f)[1 + \text{sgn}(f)]$$

or

$$X_p(f) = \begin{cases} 2X(f), & f > 0 \\ 0, & f < 0 \end{cases}$$



- We can also show that

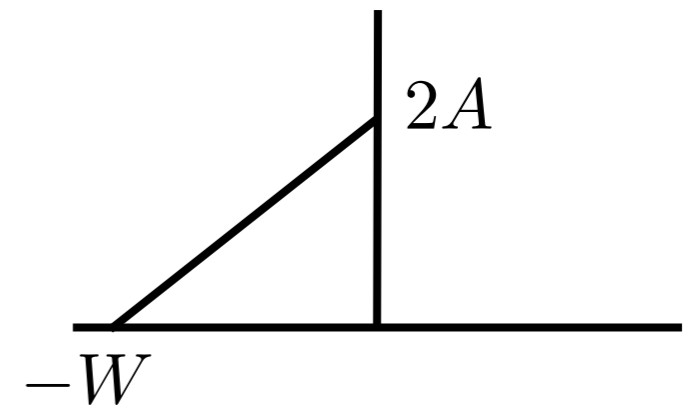
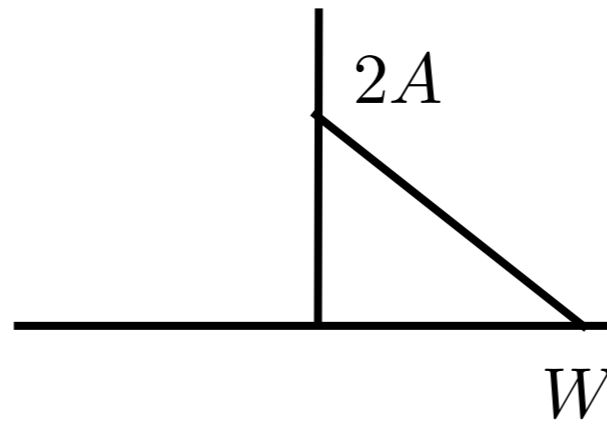
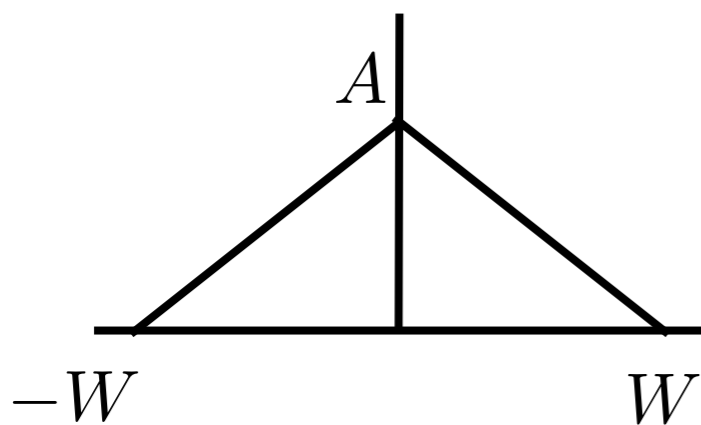
$$x_q(t) = x(t) - j\hat{x}(t)$$

and its Fourier transform

$$X_q(f) = X(f) [1 - \text{sgn}(f)]$$

$$= \begin{cases} 0, & f > 0 \\ 2X(f), & f < 0 \end{cases}$$

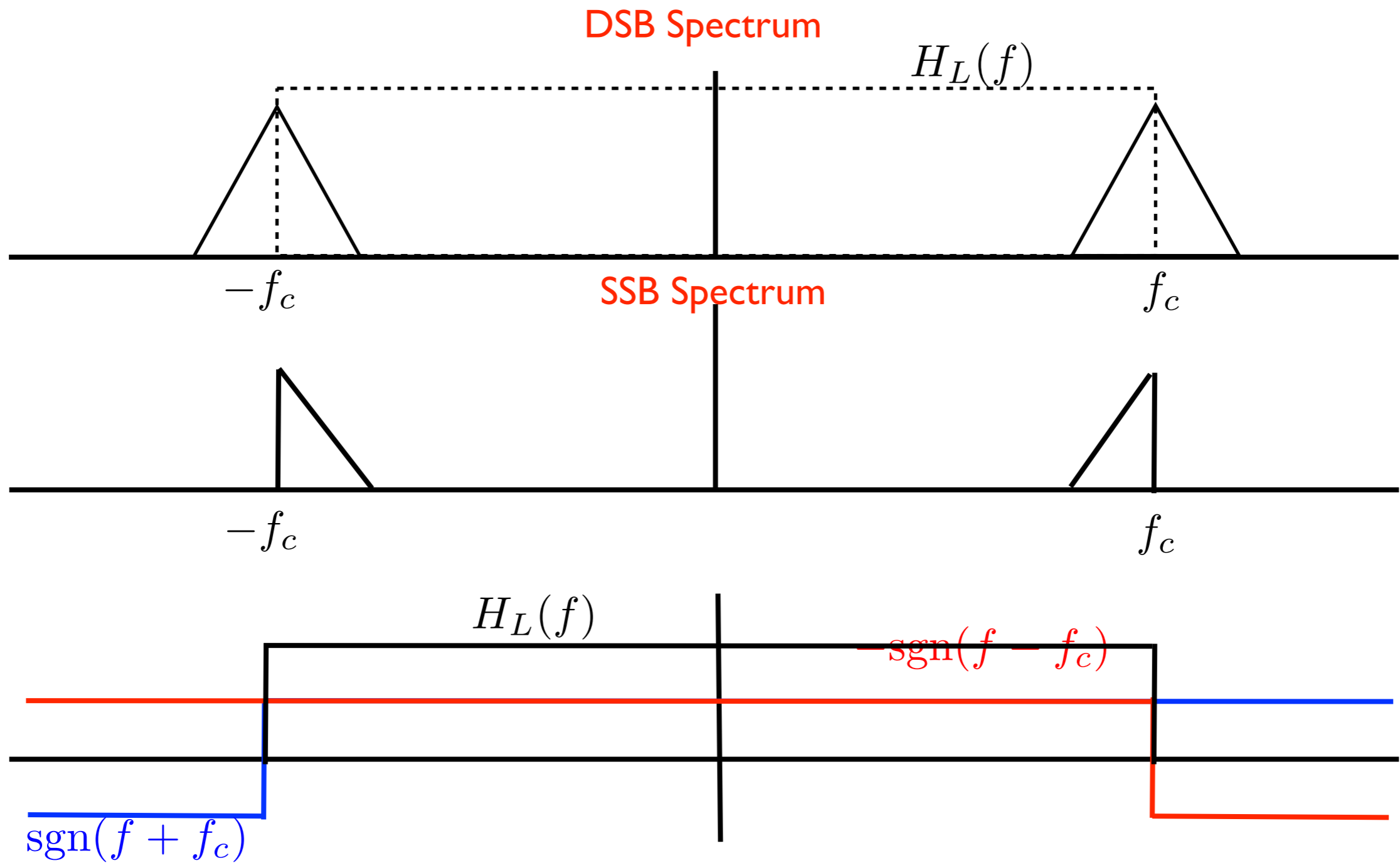
$|X(f)|$



# Single-Sideband (SSB) Modulation

- SSB modulation
  - Suppress one of the two sidebands in the DSB-SC modulated wave prior to transmission
- Method of SSB Modulations
  - Time domain expression
    - SSB signal from DSB-SC is derived using the Hilbert transform.
  - Frequency domain expression
    - SSB signal from DSB-SC is generated Analytic signal is derived using the analytic signal.

# Generation of LSB SSB



- Sideband filter

$$H_L(f) = \frac{1}{2} [\text{sgn}(f + f_c) - \text{sgn}(f - f_c)]$$

- Fourier transform of DSB-SC signal

$$S(f) = \frac{1}{2} A_c [M(f - f_c) + M(f + f_c)]$$

- Lower-Sideband SSB signal

$$S_{LSB}(f) = \frac{1}{4} A_c [M(f + f_c) \text{sgn}(f + f_c) + M(f - f_c) \text{sgn}(f + f_c)] = M(f - f_c)$$

$$- \frac{1}{4} A_c [M(f + f_c) \text{sgn}(f - f_c) + M(f - f_c) \text{sgn}(f - f_c)]$$

or

$$= -M(f + f_c)$$

$$S_{LSB}(f) = \frac{1}{4} A_c [M(f + f_c) + M(f - f_c)]$$

$$+ \frac{1}{4} A_c [M(f + f_c) \text{sgn}(f + f_c) - M(f - f_c) \text{sgn}(f - f_c)]$$

- From our study of DSB

$$\frac{1}{2}A_c m(t) \cos(2\pi f_c t) \iff \frac{1}{4}A_c [M(f + f_c) + M(f - f_c)]$$

- Also recall the Hilbert transform

$$\hat{m}(t) \iff -j \operatorname{sgn}(f) M(f), \quad \hat{m}(t) e^{\pm j2\pi f_c t} \iff -j M(f \mp f_c) \operatorname{sgn}(f \mp f_c)$$

- Thus

$$\begin{aligned} \mathcal{F}^{-1} \left\{ \frac{1}{4} A_c [M(f + f_c) \operatorname{sgn}(f + f_c) - M(f - f_c) \operatorname{sgn}(f - f_c)] \right\} \\ = -A_c \frac{1}{4j} \hat{m}(t) e^{-j2\pi f_c t} + A_c \frac{1}{4j} \hat{m}(t) e^{+j2\pi f_c t} \\ = \frac{1}{2} A_c \hat{m}(t) \sin 2\pi f_c t \end{aligned}$$

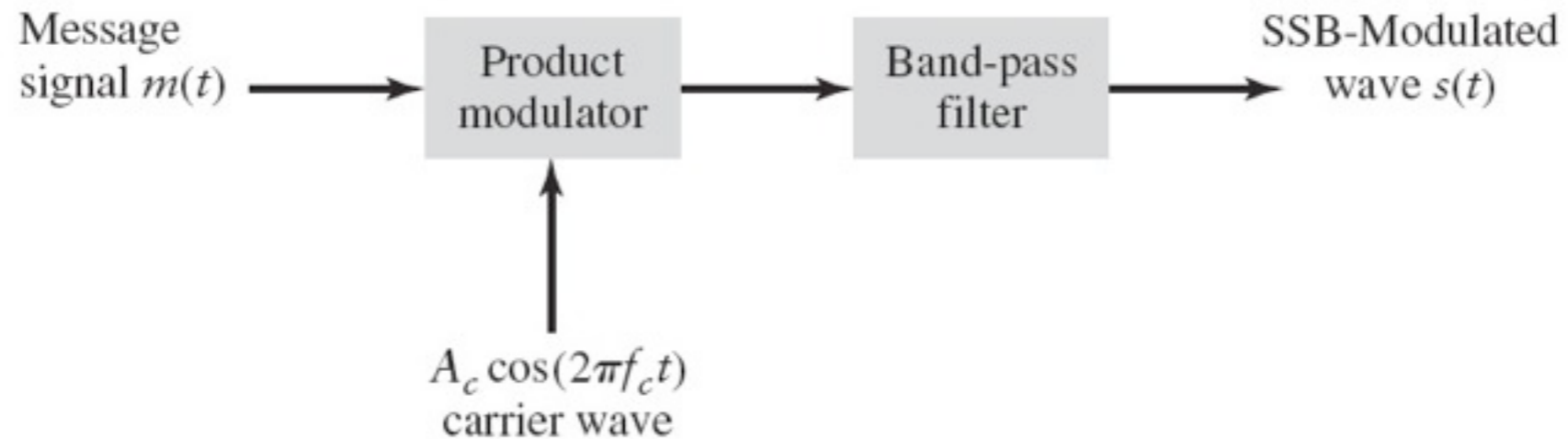
- General form of a lower-sideband SSB signal

$$s_{LSB}(t) = \frac{1}{2}A_c m(t) \cos(2\pi f_c t) + \frac{1}{2}A_c \hat{m}(t) \sin(2\pi f_c t)$$

- Similarly, we can obtain the general form of a upper-sideband SSB signal

$$s_{USB}(t) = \frac{1}{2}A_c m(t) \cos(2\pi f_c t) - \frac{1}{2}A_c \hat{m}(t) \sin(2\pi f_c t)$$

- Block diagram for implementation



**FIGURE 3.19** Frequency-discrimination scheme for the generation of a SSB modulated wave.

[Ref: Haykin & Moher, Textbook]

# SSB Generation using Analytic Signal

- The positive-frequency portion of  $M(f)$

$$M_p(f) = \frac{1}{2} \mathcal{F} [m(t) + j\hat{m}(t)]$$

- The negative-frequency portion of  $M(f)$

$$M_n(f) = \frac{1}{2} \mathcal{F} [m(t) - j\hat{m}(t)]$$

- Upper-sideband SSB signal in the frequency domain

$$S_{USB}(f) = \frac{1}{2} A_c M_p(f - f_c) + \frac{1}{2} A_c M_n(f + f_c)$$

- Inverse Fourier transform

$$s_{USB}(t) = \frac{1}{4} A_c [m(t) + j\hat{m}(t)] e^{j2\pi f_c t} + \frac{1}{4} A_c [m(t) - j\hat{m}(t)] e^{-j2\pi f_c t}$$

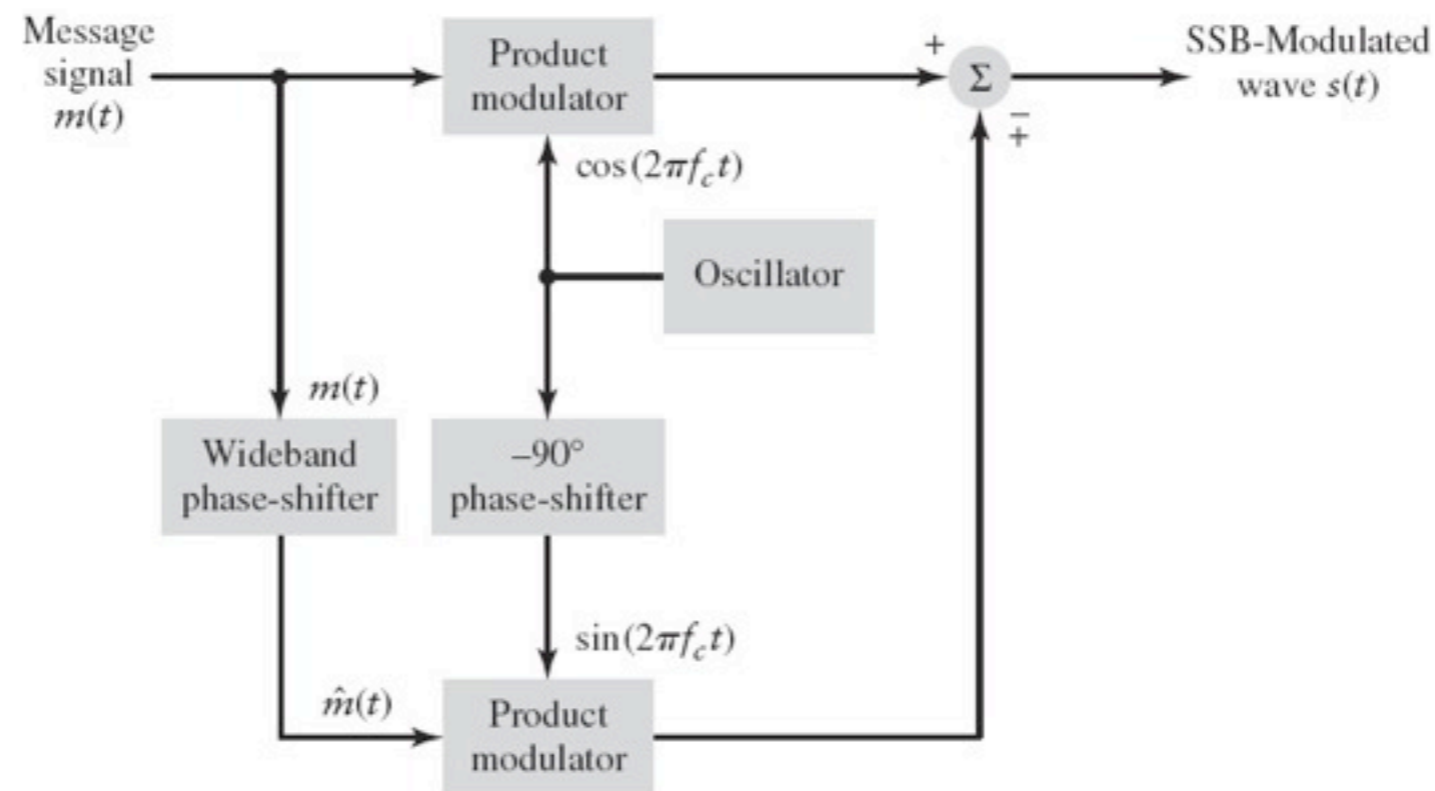
or

$$s_{USB}(t) = \frac{1}{4} A_c m(t) [e^{j2\pi f_c t} + e^{-j2\pi f_c t}] - j \frac{1}{4} A_c \hat{m}(t) [e^{j2\pi f_c t} - e^{-j2\pi f_c t}]$$



# Block Diagram for Implementation

- Wide-band phase-shifter is designed to produce the Hilbert transform in response to the incoming message signal.



**FIGURE 3.20** Phase discrimination method for generating a SSB-modulated wave.  
Note: The plus sign at the summing junction pertains to transmission of the lower sideband and the minus sign pertains to transmission of the upper sideband.

[Ref: Haykin & Moher, Textbook]

# Coherent Detection of SSB

- Synchronization of a local oscillator in the receiver with the oscillator responsible for generating the carrier in the transmitter.
- Assume that the demodulation carrier has a phase error  $\theta$

$$\begin{aligned}d(t) &= \left[ \frac{1}{2}m(t) \cos(2\pi f_c t) \pm \frac{1}{2}\hat{m}(t) \sin(2\pi f_c t) \right] \cdot \cos(2\pi f_c t + \theta) \\ &= \frac{1}{4} [m(t) \cos \theta + m(t) \cos(4\pi f_c t + \theta) \mp \hat{m}(t) \sin \theta \pm \hat{m}(t) \sin(4\pi f_c t + \theta)]\end{aligned}$$

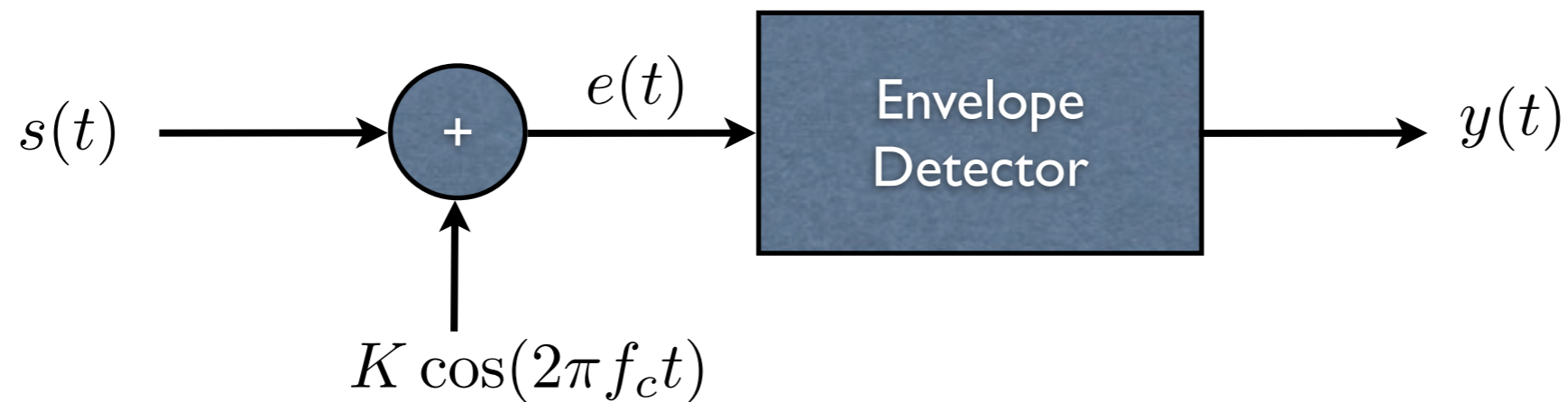
- Low-pass filtering and amplitude scaling yields

$$y(t) = m(t) \cos \theta \mp \hat{m}(t) \sin \theta$$

- For  $\theta$  equal to zero, the demodulator output is the desired message signal.

# Envelope Detector of SSB Signal (Noncoherent)

- Consider the demodulator as follows:



$$e(t) = \frac{1}{2} [A_c m(t) + K] \cos(2\pi f_c t) \pm \frac{1}{2} A_c \hat{m}(t) \sin(2\pi f_c t)$$

$$y(t) = \sqrt{\left[ \frac{1}{2} (A_c m(t) + K) \right]^2 + \left[ \frac{1}{2} A_c \hat{m}(t) \right]^2}$$

- If we set  $K$  to be

$$\left[ \frac{1}{2} A_c m(t) + K \right]^2 \gg \left[ \frac{1}{2} A_c \hat{m}(t) \right]$$

- Then,

$$y(t) \approx \frac{1}{2} A_c m(t) + K$$